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 2010
 MECHANICAL ENGINEERING - II

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9. The heat flow rate through parallel walls of thickness  $L_1$ ,  $L_2$  and  $L_3$  and having surface areas  $A_1, A_2$  and  $A_3$ , thermal conductivities  $k_1, k_2$ , and  $k_3$ , respectively and first and last walls maintained at temperatures  $t_1$  and  $t_2$  will be

(a)  

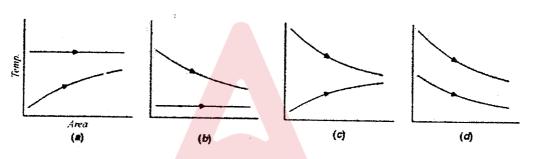
$$\frac{t_1 - t_2}{\frac{L_1}{A_1 k_1} + \frac{L_2}{A_2 k_2} + \frac{L_3}{A_3 k_3}}$$
(b)  

$$\frac{t_1 - t_2}{\frac{k_1}{A_1 L_1} + \frac{k_2}{A_2 L_2} + \frac{k_3}{A_3 L_3}}$$
(c)  

$$\frac{t_1 - t_2}{\frac{k_1 A_1}{L_1} + \frac{k_2 A_2}{L_2} + \frac{k_3 A_3}{A_3 L_3}}$$
(d)  

$$\frac{t_1 - t_2}{\frac{L_1 A_1}{L_1} + \frac{L_2}{L_2} + \frac{L_3}{L_3}}$$

- 10. Which of the following property of air does not increase with rise in temperature?
  - (a) Specific gravity (b) Kinematic viscosity (c) Thermal conductivity (d) Thermal diffusivity
- 11. Choose the correct figure representing gas to gas heat transfer in parallel flow heat exchanger?



12. The value of Prandtl number for air is about

- 13. A body cools from 90°C to 80°C in 5 minutes. Under the same external conditions to cool from 80°C to 70°C the body will take
  (a) 5 minutes
  (b) 4 minutes
  (c) 2.5 minutes
  (d) More than 5 minutes
- 14. When the temperature of a solid surface changes from  $227^{\circ}C$  to  $1227^{\circ}C$ , its total emissive power changes from  $E_1$  to  $E_2$ . The ratio  $\left(\frac{E_2}{E_1}\right)$  will be

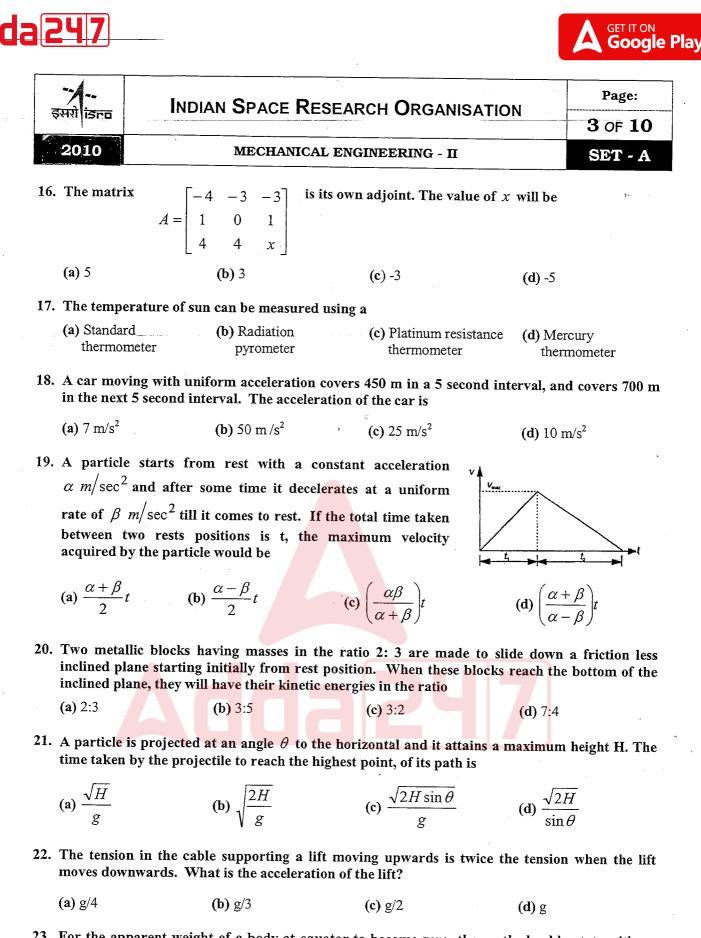
(a) 3 (b) 9 (c) 81 (d) Cannot be determined on the basis of information provided

(c)  $C_{p} - C_{v}$ 

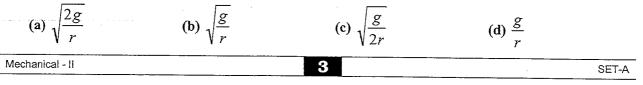
(d)  $C_{p} + C_{v}$ 

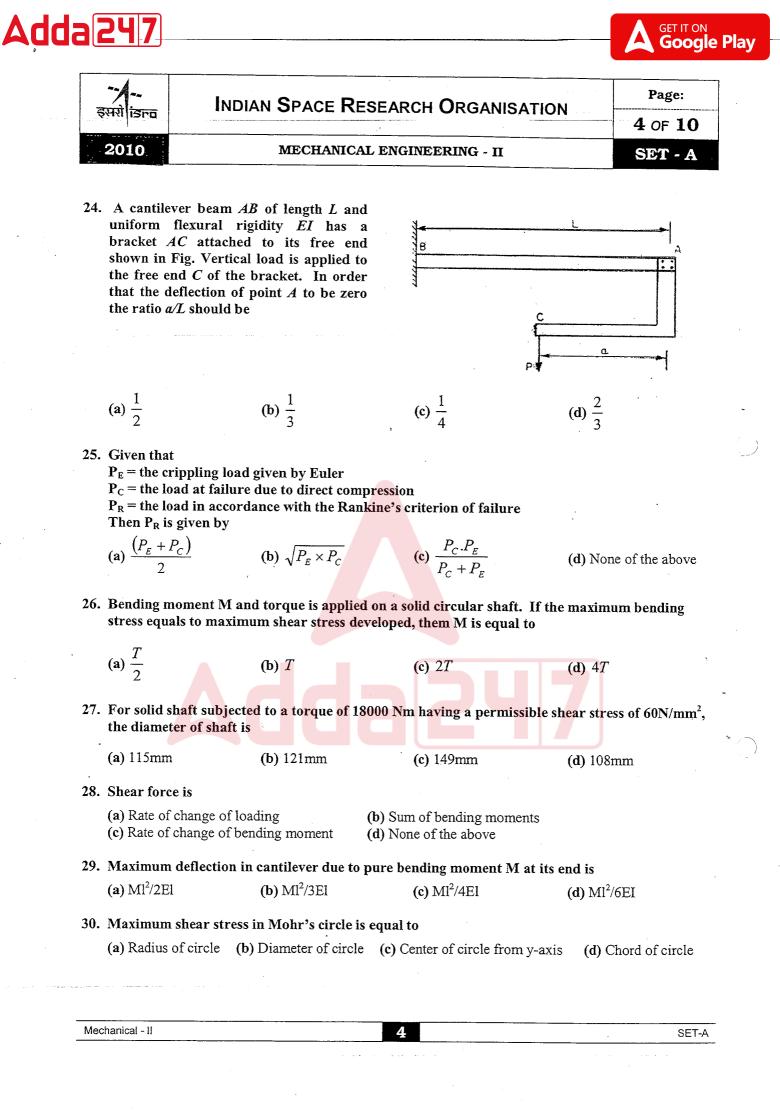
15. Characteristic gas constant of a gas is equal to

(a) 
$$C_p / C_v$$
 (b)  $C_v / C_p$ 



23. For the apparent weight of a body at equator to become zero, the earth should rotate with an angular velocity of

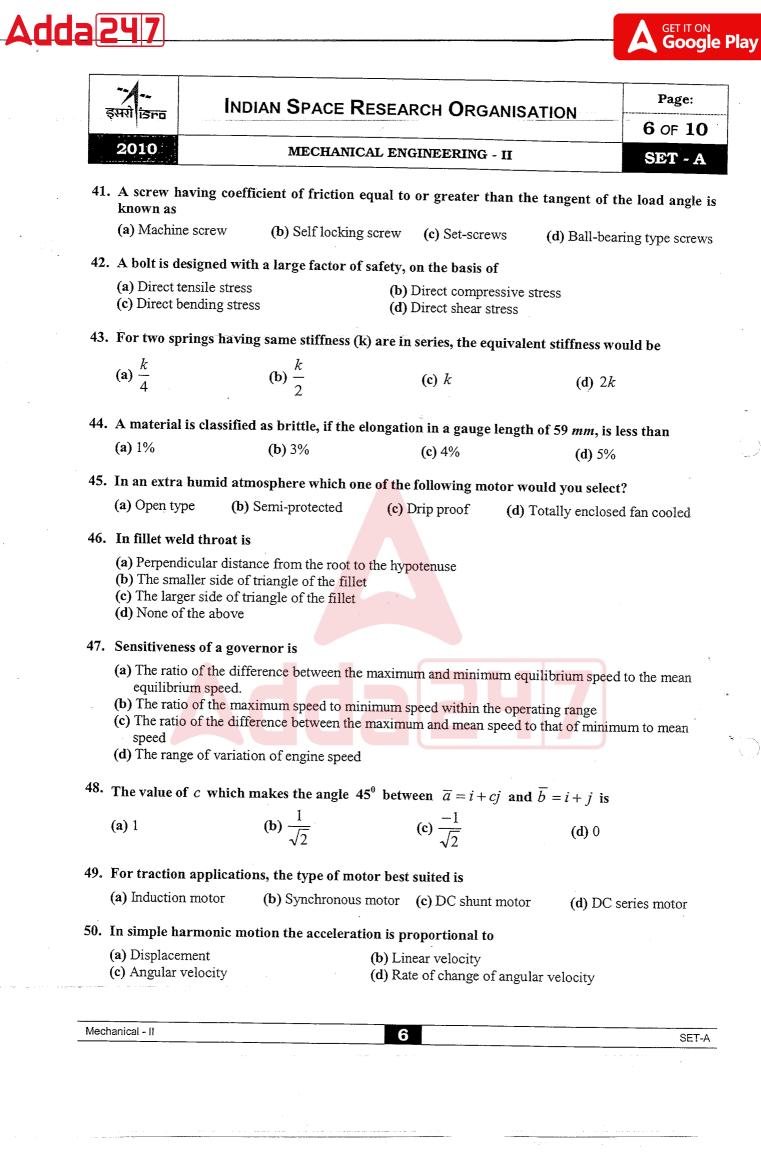




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	2010		MEC	HANICAL E	NGINEERING - II		SET ·
31.	Hardne	ess of stee	el depends on				
	• •	ount of ca hod of fal	rbon it contains prication		shape and distribution itents of alloying eler		s in iron
32.	The mo	odulus of	$1 + \cos \alpha + i \sin \alpha$	χ is			
	<b>(a)</b> 2 sin	$n\frac{\alpha}{2}$	<b>(b)</b> 2 cos	$\frac{\alpha}{2}$	(c) $\sin^2 \frac{\alpha}{2} - 1$	( <b>d</b> ) cos	$s^2 \frac{\alpha}{2} - 1$
33.	Hardne	es of mar	tensite is about	···· ·· ·			
	(a) RC (	65	<b>(b)</b> RC 4	8	(c) RC 57	( <b>d</b> ) RC	80
34.	Materia	als after o	cold working are	subjected to	following process to	o relieve stresses	5
		working	(b) Temp		(c) Normalizing	(d) Ann	
35.	In drop	o forging	the forging is do	ne by			
26	(d) Dro	opping a w	die with hammer veight on hammer achine tools can b	to produce re	equisite impact		
30.	1.	Lathe	machine				
30.	1. 2. 3.	Drilling Vertical	machine milling machine tal milling mach <mark>i</mark>	ne			
30.	1. 2. 3.	Drilling Vertical Horizon	milling machine	ne	(c) 2 and 4	<b>(d)</b> 1 ar	nd 2
	1. 2. 3. 4. (a) 1,2,3 The ver	Drilling Vertical Horizon	milling machine tal milling machi (b) 1,3,4		(c) 2 and 4 s face value before a		
	1. 2. 3. 4. (a) 1,2,3 The ver for	Drilling Vertical Horizon	milling machine tal milling machi (b) 1,3,4 ling should not b	e taken at it	s face value before a	n actual check	has been t
	1. 2. 3. 4. (a) 1,2,3 The ver	Drilling Vertical Horizon	milling machine tal milling machi (b) 1,3,4	e taken at it		n actual check	has been t rature
37.	1. 2. 3. 4. (a) 1,2,3 The ver for (a) Zero	Drilling Vertical Horizon a rnier read	milling machine tal milling machi (b) 1,3,4 ling should not b	e taken at it n (c) Flat	s face value before a ness of measuring jav	n actual check (d) Tempe	has been t rature
37.	1. 2. 3. 4. (a) 1,2,3 The ver for (a) Zero	Drilling Vertical Horizon anier read o error	milling machine tal milling machi (b) 1,3,4 ding should not b (b) Its calibration	e taken at it (c) Flat percentage	s face value before a ness of measuring jav	n actual check vs (d) Tempe equaliz	has been t rature
37.	1. 2. 3. 4. (a) 1,2,3 The ver for (a) Zerco High ca (a) 0.1 t	Drilling Vertical Horizon anier read o error arbon stee to 0.3%	milling machine tal milling machi (b) 1,3,4 ding should not b (b) Its calibration el carries carbon (b) 0.3 to	e taken at it (c) Flat percentage	s face value before a ness of measuring jav of	n actual check vs (d) Tempe equaliz (d) 0.8	has been t rature ation to 1.5%
37.	1. 2. 3. 4. (a) 1,2,3 The ver for (a) Zerco High ca (a) 0.1 t In orde (a) Acou	Drilling Vertical Horizon anier read o error arbon stee to 0.3%	milling machine tal milling machi (b) 1,3,4 ding should not b (b) Its calibration el carries carbon (b) 0.3 to sure/detect mater ssion	e taken at it (c) Flat percentage 0.6% ials by non-	s face value before a ness of measuring jav of (c) 0.6 to 0.8%	n actual check vs (d) Tempe equaliz (d) 0.8 he method gener	has been t rature ation to 1.5%
37. 38. 39.	1. 2. 3. 4. (a) 1,2,3 The ver for (a) Zero High ca (a) 0.1 t In orde (a) Acou (c) Liqu	Drilling Vertical Horizon and crnier read o error arbon stee to 0.3% or to meas ustic emis ustic emis did crystal	milling machine tal milling machi (b) 1,3,4 ding should not b (b) Its calibration el carries carbon (b) 0.3 to sure/detect mater ssion	e taken at it (c) Flat percentage 0.6% fials by non-	s face value before a ness of measuring jav of (c) 0.6 to 0.8% destructive testing th b) Infrared radiometer	n actual check vs (d) Tempe equaliz (d) 0.8 he method gener	has been t rature ation to 1.5%

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	201	0		MECH	ANICAL E	CNGINEERING - II	SET - A
51.	. A vi	bro mete	r				
				. 1:4 J -		· • • • • • •	
			vibration ap mature of v		(b) (d)	Indicates vibration frequency Only indicates second and at	/ pove harmonics
52.	At n	ode of th	ie shaft				
	(a) ]	The vibrat	tions are mi	nimum	<b>(b)</b> The	e vibrations are maximum	
	(c) T	he vibrat	ions are av	erage		e vibrations are zero	
53.	List A. M B. H C. R	1 (Match Ialleabil Iardness Resilience	1 property <sub>.</sub> lity	and select t	Lis 1. Wi 2. Im 3. Co	t answer using the codes.giv st II (Related to) ire drawing pact loads ld rolling	ven below the lists.
	<b>D.</b> 19	sotropy				lentation	
		А	В	С	5. Dir D	ection	
	(a)	4	2	1	3		
	(b)	3	4	2	5		
	(c)	5	4	2	3		
	(d)	3	2	1	5		
54.	The	cutting s	peed of the	e tool in a m	lechanical	shaper is	
	(b) N (c) N	Aaximum Iaximum	at the end at the midd	nning of the of the cuttin dle of the cu dle of the cu	g stroke tting stroke		
55.	Whi	ch is not	correct sta	itement abo	ut the fun	ction of flux in brazing	
	(a) T (b) T (c) T bi	o avoid t o dissolv o prevent azing ma	hermal dist e surface o t oxides fro uterial	ortion and c xide coating m forming d	racking s which ha uring the b	we formed prior to brazing brazing operation on both the l	base metal and the
56					by reducing	g the viscosity of the melt	
	(a) S (b) M (c) S	hapes wh Iass prod hapes wh	uction ich are very	le by difficu	nd intricate	omplex patterns in sand castir e and can't be cast by any othe	-
57.	Inter	nal and o	external th	reads can b	e produce	d on tapered surfaces conve	niently by
	<b>(a)</b> U	niversal r	nilling mac nilling mac	hine (b)	Plano mill lathe		
					•		
Mer	hanical	- 11				7	
	. ioninoal	**				7	SET-A





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÷	2010		MECHAN	[CAL E]	NGINEERING - II		SET - A
58.	Optical squa	are is					
	<ul><li>(b) A constant ray, equal</li><li>(c) A constant ray, equal</li></ul>	nt deviati to 90° nt deviati to 45°	•	he angle ne angle	t at 90 <sup>0</sup> of deviation between of deviation between		
59	A master ga	uge is					
	(c) A standar	ational re d gauge	eference standard for checking accur experienced techni		auges used on shop f	loors	
60.	Dimension o	f the hole	e is $50^{+0.02}_{-0.00}$ m	, im and :	shaft is $50^{+0.02}_{+0.00}$ m	nm. The mini	mum clearance
	is						
	(a) 0.02 mm		<b>(b)</b> 0.00 mm		(c) -0.02 mm	( <b>d</b> ) 0.0	01 mm
61.	Two cutters	are mou	nted on the arbo	r so that	two faces are machi	ined simultan	eously in
	(a) Gang mill	ing	(b) Straddle n	uilling	(c) Pendulum mil	ling (d) Pr	ofile milling
62.	The main all	oving ele	ements in high sn	eed stee	l in order of increasi	ing proportion	ara
	<ul><li>(a) Vanadium</li><li>(c) Chromiun</li></ul>	i, chromi	um, tungsten		(b) Tungsten, titaniur (d) Tungsten, chromi	n, vanadium	
63.	Surface roug	hness on	a dra <mark>wi</mark> ng is r <mark>e</mark> r	resente	d by		
	(a) Triangles		(b) Circles		(c) Squares	( <b>d</b> ) Re	ectangles
64	A husband a	nd wife	nn <sup>*</sup> on in on into				
			1		<mark>r two vacanc</mark> ies for s bility of wife getting	1	
			5 ne of them gettin		· · ·	7	· I nen the
		uat anyo	-	ig select	1	34	4
	(a) $\frac{11}{35}$		<b>(b)</b> $\frac{12}{35}$		(c) $\frac{1}{35}$	(d) $\frac{34}{32}$	5
65.	Cylindrical p	arts are	held on planer b	У		,	
	<ul><li>(a) V-blocks</li><li>(c) V-block, 7</li></ul>	and arres	tors	(b	) Angle plates ) T-bolt and clamps		
66.	Expressing a	ı dimens	ion as 25.3 <sup>±0.05</sup> m	m is the	case of		
	(a) Unilatera (c) Limiting			•	) Bilateral tolerance ) All of the above		
Mech	nanical - II				8		SET

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	র	••• सरो isra	INDIAN SPACE RESE	ARCH ORGANISAT	ION Page:
			MECHANICALE	NGINEERING - II	9 OF 10
		2010			SET - A
	67.	In comparison to	o an open-loop system a close	d loop system is	
		(a) More stable	(b) More accurate	(c) More complex	(d) All of the above
	68.		gram is shown in Fig. The fri w in a smooth pipe is given b		
		(a) A	<b>(b)</b> B		C C
		(c) E	(d) C		R <sub>e</sub>
	69.	750 m and 600 n	consists of three pipes arran n and diameters 750 mm, 600 ystem to an equivalent 450 m	) mm, 450 mm respectiv	
		<b>(a)</b> 671.3m	<b>(b)</b> 771.3m	(c) 871.3m	<b>(d)</b> 971.3m
	70.	Friction drag is	generally larger than the pre	ssure drag in	
		(a) Flow past a sphere	(b) Flow past a thin she	et (c) Flow past an airfoil	(d) Flow past a cylilnde
	71.	If D is the diame	eter of impeller at <mark>inlet, w is</mark>	the width of impeller at	inlet and $V_f$ is the velocity
			hen discharge t <mark>hrough a cen</mark>		•
		(a) $\pi DV_f$	(b) $DV_f w$	(c) $\pi DV_f W$	(d) $\pi Dw$
	72.	Cavitation para	meter is defined by		
		(a) $\frac{P_v - P}{\rho V^2 / 2}$	(b) $\frac{P_{atm} - P_v}{\rho V^2 / 2}$	(c) $\frac{P-P_{atm}}{P-P_{atm}}$	(d) $\frac{P-P_{v}}{P-P_{v}}$
		$\rho V^2/2$	$\rho V^{2}/2$	(c) $\frac{P - P_{atm}}{\rho V^2}$	(d) $\frac{P - P_v}{\rho V^2}$
			, ,	2	2
	73.	The maximum t	hickness of boundary layer in	n a pipe of radius R is	
		(a) 0.1 R	<b>(b)</b> 0.22 R	(c) 0.5 R	(d) R
	74.		a pipe lilne carrying water, th At a point B, 2 m higher tha flow would be		
		(a) A to B (b)	B to A (c) Cannot be asce	ertained from data	(d) None of these
4 N. M. S.					

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	2010	MECHANIC	AL ENGINEERING - II		SET - A
75	. In the given	figure pressure $p$ , in $kPa$ ,	is		· • •
				Hgl(S=13.6)	30cm
	<b>(a)</b> 37	<b>(b)</b> 48.0	(c) 45.2	( <b>d</b> ) 51.3	( <u>*****</u> )
76.	A small pla dumped inte	stic boat loaded with piece o the water allowing the boa	s of steel rods is floating t to float empty, the wate	g in a bathtub. I er level in the tub	f the cargo will
	(a) Rise	(b) Fall (c) Not ch:			
77.	Four cars, v How far, in (	vith a mass of 1500 kg each cm will it sink in the water?	, are loaded on a 6 m w	ide, 12 m long sm	all car ferr
	<b>(a)</b> 15.2	<b>(b)</b> 11.5	<b>(c)</b> 10.2	(d) 8.3	
78.	Water enter reach before	s a turbine at 900kPa with r it enters the turbine rotor?	egligible velocity. What	maximum speed,	in m/s, can
					•
	(a) 42	<b>(b)</b> 47	(c) 45	<b>(d)</b> 52	
79.	Given that: Specific grav Intensity of J	vity of mercury = 13.6; pressure = 40kPa		( <b>d</b> ) 52	
79.	Given that: Specific grav Intensity of p Express the i	vity of mercury = 13.6;	in various units (S.I) (b) 0.4 bar, 4.077	( <b>d</b> ) 52 ' m of water, 0.299	m of
79. 80.	Given that: Specific grav Intensity of p Express the i (a) 0.3 bar, 3. (c) 0.5 bar, 5. mercury	vity of mercury = 13.6; pressure = 40kPa intensity of pressure (gauge)	in various units (S.I) ercury (b) 0.4 bar, 4.077 mercury (d) None of the a	' m of water, 0.299	m of
	Given that: Specific grav Intensity of p Express the i (a) 0.3 bar, 3. (c) 0.5 bar, 5. mercury The differen (a) $\frac{d^2 y}{dx^2} + 5\frac{d^2 y}{dx^2}$	wity of mercury = 13.6; pressure = 40kPa intensity of pressure (gauge) 077 m of water, 0.15 m of me 077 m of water, 0.339 m of tial equation satisfying $y =$ $\frac{dy}{dx} - 6y = 0$	in various units (S.I) ercury (b) 0.4 bar, 4.077 mercury (d) None of the a	' m of water, 0.299	m of
	Given that: Specific grav Intensity of p Express the i (a) 0.3 bar, 3. (c) 0.5 bar, 5. mercury The differen	wity of mercury = 13.6; pressure = 40kPa intensity of pressure (gauge) 077 m of water, 0.15 m of me 077 m of water, 0.339 m of tial equation satisfying $y =$ $\frac{dy}{dx} - 6y = 0$	in various units (S.I) frcury (b) 0.4 bar, 4.077 mercury (d) None of the a $Ae^{3x} + Be^{2x}$ is	' m of water, 0.299 bove	m of
	Given that: Specific grav Intensity of p Express the i (a) 0.3 bar, 3. (c) 0.5 bar, 5. mercury The differen (a) $\frac{d^2 y}{dx^2} + 5\frac{d^2 y}{dx^2}$	wity of mercury = 13.6; pressure = 40kPa intensity of pressure (gauge) 077 m of water, 0.15 m of me 077 m of water, 0.339 m of tial equation satisfying $y =$ $\frac{dy}{dx} - 6y = 0$	in various units (S.I) frecury (b) 0.4 bar, 4.077 mercury (d) None of the a $Ae^{3x} + Be^{2x}$ is (b) $\frac{d^2y}{dx^2} - 5\frac{dy}{dx} + 6y$	' m of water, 0.299 bove	m of
	Given that: Specific grav Intensity of p Express the i (a) 0.3 bar, 3. (c) 0.5 bar, 5. mercury The differen (a) $\frac{d^2 y}{dx^2} + 5\frac{d^2 y}{dx^2}$	wity of mercury = 13.6; pressure = 40kPa intensity of pressure (gauge) 077 m of water, 0.15 m of me 077 m of water, 0.339 m of tial equation satisfying $y =$ $\frac{dy}{dx} - 6y = 0$	in various units (S.I) frecury (b) 0.4 bar, 4.077 mercury (d) None of the a $Ae^{3x} + Be^{2x}$ is (b) $\frac{d^2y}{dx^2} - 5\frac{dy}{dx} + 6y$	' m of water, 0.299 bove	m of
	Given that: Specific grav Intensity of p Express the i (a) 0.3 bar, 3. (c) 0.5 bar, 5. mercury The differen (a) $\frac{d^2 y}{dx^2} + 5\frac{d^2 y}{dx^2}$	wity of mercury = 13.6; pressure = 40kPa intensity of pressure (gauge) 077 m of water, 0.15 m of me 077 m of water, 0.339 m of tial equation satisfying $y =$ $\frac{dy}{dx} - 6y = 0$	in various units (S.I) frecury (b) 0.4 bar, 4.077 mercury (d) None of the a $Ae^{3x} + Be^{2x}$ is (b) $\frac{d^2y}{dx^2} - 5\frac{dy}{dx} + 6y$	' m of water, 0.299 bove	m of
	Given that: Specific grav Intensity of p Express the i (a) 0.3 bar, 3. (c) 0.5 bar, 5. mercury The differen (a) $\frac{d^2 y}{dx^2} + 5\frac{d^2 y}{dx^2}$	wity of mercury = 13.6; pressure = 40kPa intensity of pressure (gauge) 077 m of water, 0.15 m of me 077 m of water, 0.339 m of tial equation satisfying $y =$ $\frac{dy}{dx} - 6y = 0$	in various units (S.I) frecury (b) 0.4 bar, 4.077 mercury (d) None of the a $Ae^{3x} + Be^{2x}$ is (b) $\frac{d^2y}{dx^2} - 5\frac{dy}{dx} + 6y$	' m of water, 0.299 bove	m of